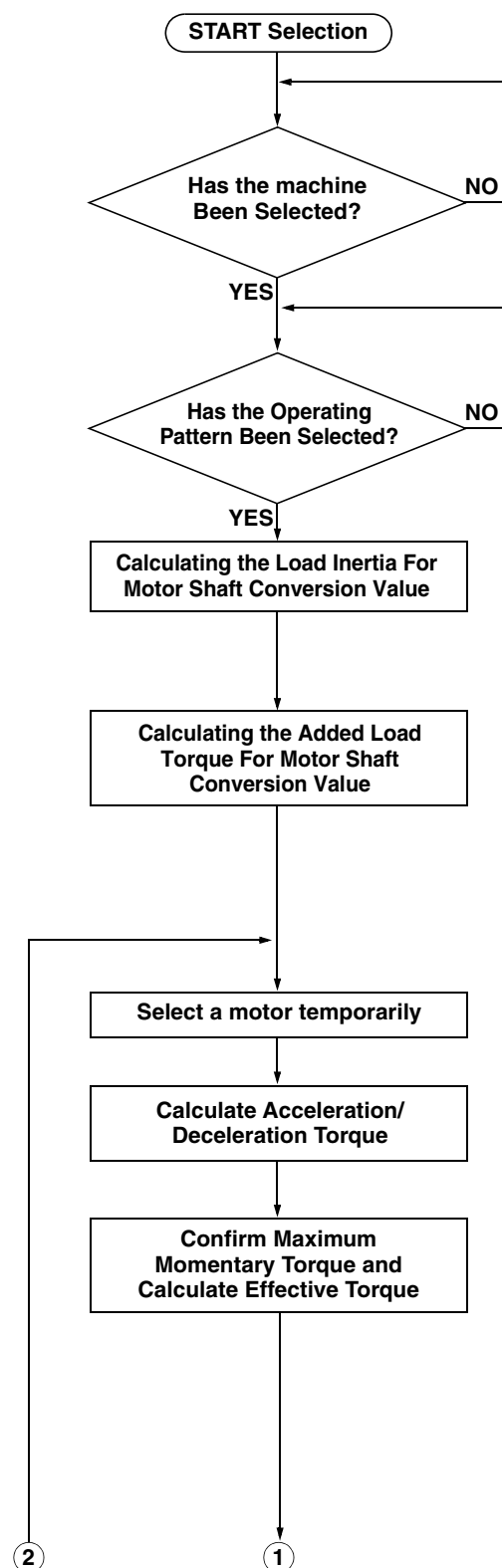
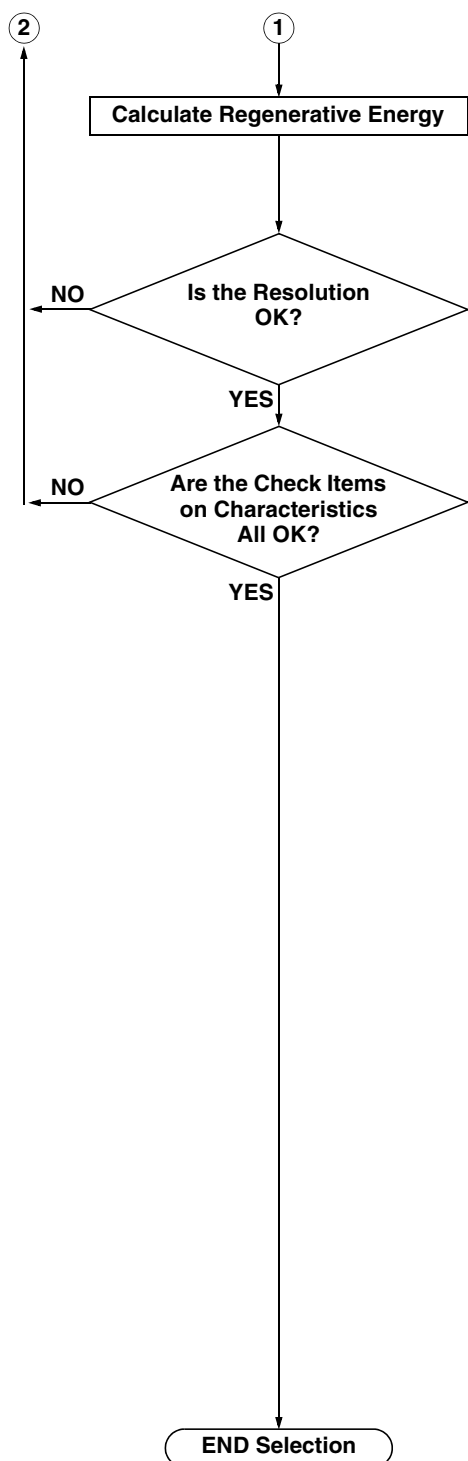


Servo Motor Selection Flow Chart



Explanation	References
<ul style="list-style-type: none"> Determine the size, mass, coefficient of friction, and external forces of all the moving part of the Servo Motor the rotation of which affects. 	---
<ul style="list-style-type: none"> Determine the operating pattern (relationship between time and speed) of each part that must be controlled. Convert the operating pattern of each controlled element into the motor shaft operating pattern. 	• Operation Pattern Formula
<ul style="list-style-type: none"> The elements of the machine can be separated so that inertia can be calculated for each part that moves as the Servo Motor rotates. Calculate the inertia applied to each element to calculate the total load inertia of the motor shaft conversion value. 	• Inertia Formulas
<ul style="list-style-type: none"> Calculation of Friction Torque Calculates the frictional force for each element, where necessary, and converts it to friction torque for a motor shaft. Calculation of External Torque Calculates the external force for each element, where necessary, and converts it to external torque of a motor shaft. Calculates the total load torque for the motor shaft conversion value. 	• Load Torque Formulas
<ul style="list-style-type: none"> Select a motor temporarily based upon the motor shaft converted load inertia, friction torque, external torque and r.p.m of a motor. 	---
<ul style="list-style-type: none"> Calculate the Acceleration/Deceleration Torque from the Load Inertia or Operating Pattern. 	• Acceleration/Deceleration Torque Formulas
<ul style="list-style-type: none"> Calculate the necessary torque for each part of the Operating Pattern from the Friction Torque, External Torque and Acceleration/Deceleration Torque. Confirm that the maximum value for the Torque for each operating part (Maximum Momentary Torque) is less than the Maximum Momentary Torque of the motor. Calculate the Effective Torque from the Torque for each Operating part, and confirm that it is less than the Rated Torque for the motor. 	• Calculation of Maximum Momentary Torque, Effective Torque



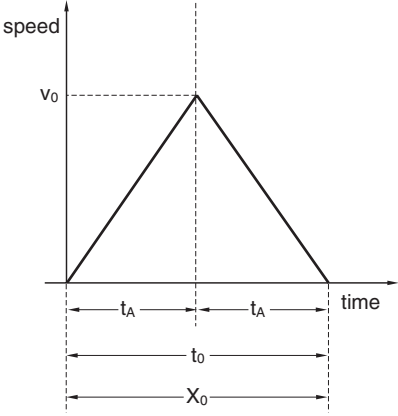
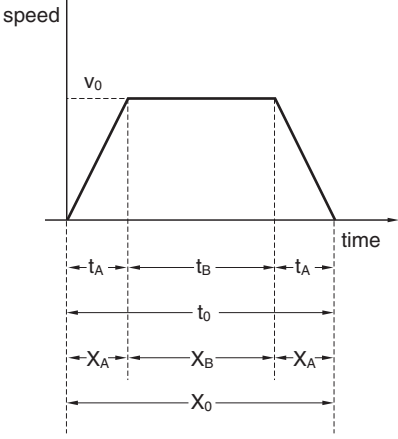
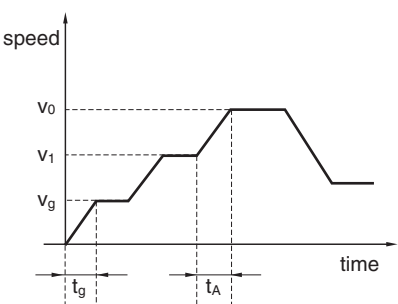
Explanation	References
• Calculate Regenerative Energy from the Torque of all the moving parts.	• Please see the user manual of each product for the details on calculation of the regenerative energy.
• Check if the the number of encoder pulses meets the system specified resolution.	• Accuracy of Positioning
• Check if the calculation meets the specifications of the temporarily selected motor. If not, change the temporarily selected motor and re-calculate it.	• The following table

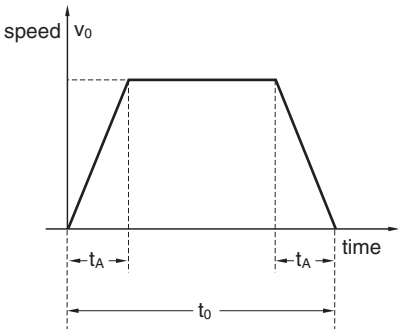
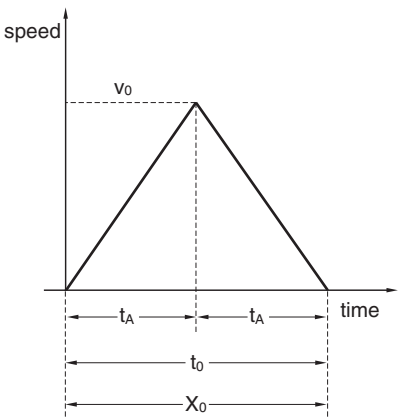
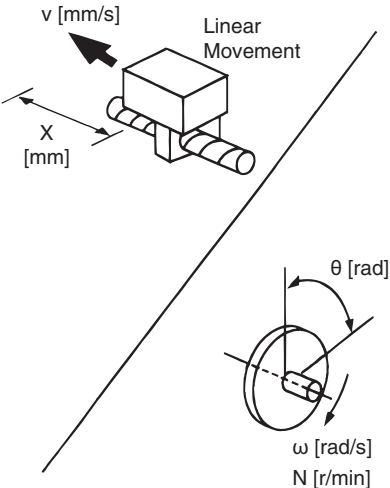
Specialized Check Items	Check Items
Load Inertia	$\text{Load Inertia} \leq \text{Motor Rotor Inertia} \times \text{Applicable Inertia Ratio}$
Effective Torque	Effective Torque < Motor Rated Torque • Please allow a margin of about 20%. *
Maximum Momentary Torque	Maximum Momentary Torque < Motor Maximum Momentary Torque • Please allow a margin of about 20%. * • For the motor Maximum Momentary Torque, use the value that is combined with a driver and the one of the motor itself.
Maximum Rotation Speed	Maximum Rotation Speed \leq Rated Rotation Speed of a motor • Try to get as close to the motor's rated rotations as possible. It will increase the operating efficiency of a motor. • For the formula, please see " Straight-line Speed and Motor Rotation Speed " on Page 11.
Regenerative Energy	Regenerative Energy \leq Regenerative Energy Absorption of a motor • When the Regenerative Energy is large, connect a Regenerative Energy Absorption Resistance to increase the Absorption capacity of the driver.
Encoder Resolution	Ensure that the Encoder Resolution meets the system specifications.
Characteristics of a Positioner	Check if the Pulse Frequency does not exceed the Maximum Response Frequency or Maximum Command Frequency of a Positioner.
Operating Conditions	Ensure that values of the ambient operating temperature/humidity, operating atmosphere, shock and vibrations meet the product specifications.

* When handling vertical loads and a load affected by the external torque, allow for about 30% of capacity.

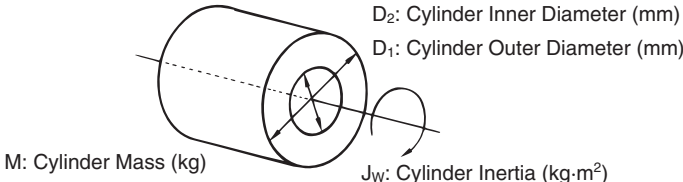
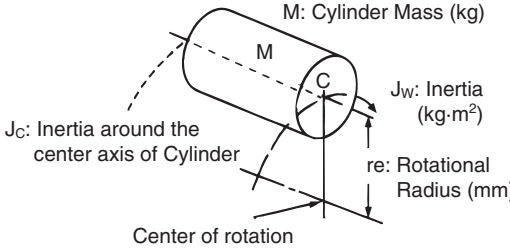
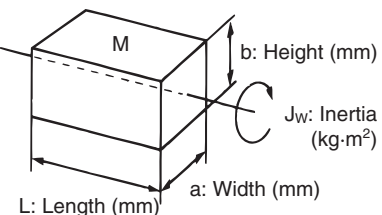
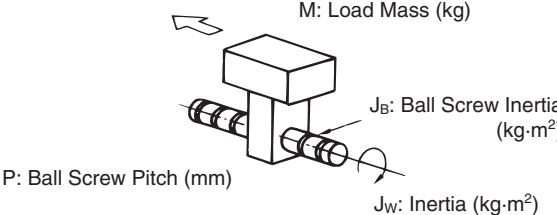
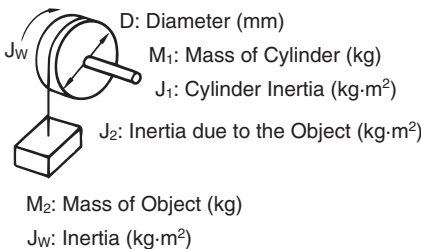
Formulas

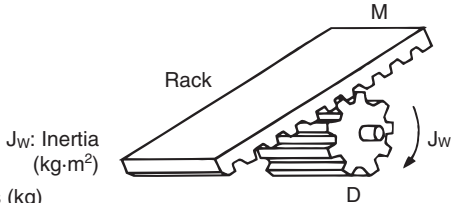
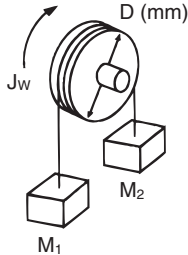
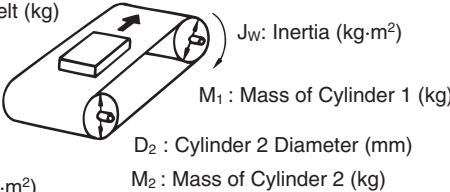
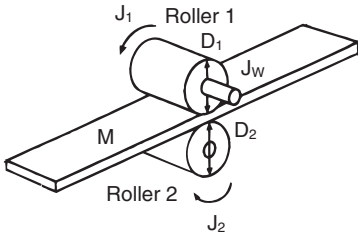
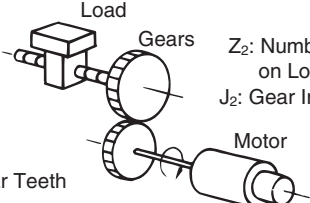
Formulas for Operating Patterns

<p>Triangular</p>	 <p>A speed-time graph for a triangular profile. The vertical axis is labeled 'speed' and the horizontal axis is labeled 'time'. The graph starts at the origin (0,0), rises linearly to a peak speed v_0 at time t_A, and then falls linearly back to zero speed at time $2t_A$. The total time is t_0. The total distance traveled is X_0. Dashed lines indicate the peak speed v_0 and the time intervals t_A, t_0, and X_0.</p>	<p>Maximum Speed $v_0 = \frac{X_0}{t_A}$ X_0: Distance Moved in t_0 Time (mm) v_0: Maximum Speed (mm/s)</p> <p>Acceleration/Deceleration Time $t_A = \frac{X_0}{v_0}$ t_0: Positioning Time (s) t_A: Acceleration/Deceleration Time (s)</p> <p>Travel Distance $X_0 = v_0 \cdot t_A$</p>
<p>Trapezoid</p>	 <p>A speed-time graph for a trapezoidal profile. The vertical axis is labeled 'speed' and the horizontal axis is labeled 'time'. The graph starts at the origin (0,0), rises linearly to a peak speed v_0 at time t_A, remains constant at v_0 for a time interval t_B, and then falls linearly back to zero speed at time $2t_A + t_B$. The total time is t_0. The total distance traveled is X_0. Dashed lines indicate the peak speed v_0 and the time intervals t_A, t_B, t_0, and the distance intervals X_A, X_B, and X_0.</p>	<p>Maximum Speed $v_0 = \frac{X_0}{t_0 - t_A}$</p> <p>Acceleration/Deceleration Time $t_A = t_0 - \frac{X_0}{v_0}$</p> <p>Total Travel Time $t_0 = t_A + \frac{X_0}{v_0}$</p> <p>Constant-velocity travel time $t_B = t_0 - 2 \cdot t_A = 2 \frac{2 \cdot X_0}{v_0} - t_0 = \frac{X_0}{v_0} - t_A$</p> <p>Total Travel Distance $X_0 = v_0 (t_0 - t_A)$</p> <p>Acceleration/Deceleration Travel Distance $X_A = \frac{v_0 \cdot t_A}{2} = \frac{v_0 \cdot t_0 - X_0}{2}$</p> <p>Constant-velocity travel distance $X_B = v_0 \cdot t_B = 2 \cdot X_0 - v_0 \cdot t_0$</p>
<p>Speed and Slope When Ascending</p>	 <p>A speed-time graph showing a multi-stage acceleration profile. The vertical axis is labeled 'speed' and the horizontal axis is labeled 'time'. The graph starts at the origin (0,0), rises linearly to speed v_g at time t_g, remains constant at v_g for a short time, then rises linearly to speed v_1, remains constant at v_1 for a short time, then rises linearly to speed v_0, remains constant at v_0 for a short time, and finally falls linearly back to zero speed. The time interval t_A is marked for the final acceleration phase. The speed gradient α is indicated as $\alpha = \frac{v_g}{t_g}$.</p> <p>Speed Gradient $\alpha = \frac{v_g}{t_g}$</p>	<p>Ascending Time $t_A = \frac{v_0 - v_1}{\alpha}$</p> <p>Ascending Time (t_A) including distance moved</p> $X_A = \frac{1}{2} \alpha \cdot t_A^2 + v_1 \cdot t_A$ $= \frac{1}{2} \frac{(v_0 - v_1)^2}{\alpha} + v_1 \cdot t_A$ <p>Speed after Ascending $v_0 = v_1 + \alpha \cdot t_A$</p>

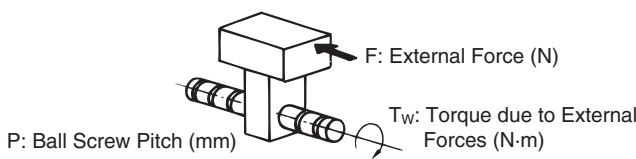
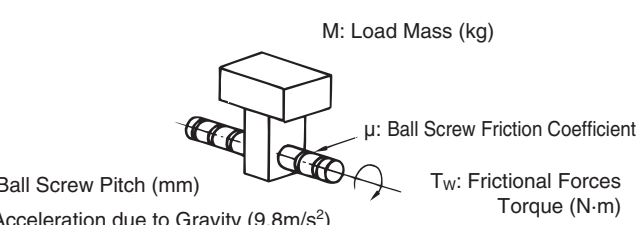
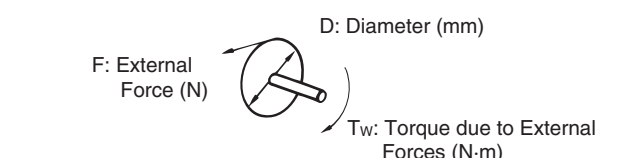
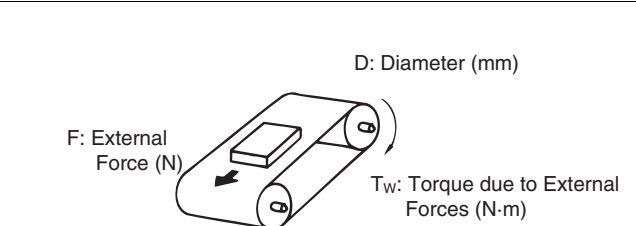
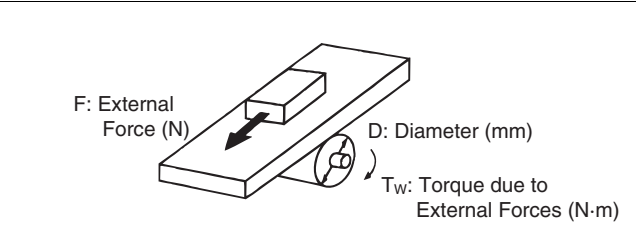
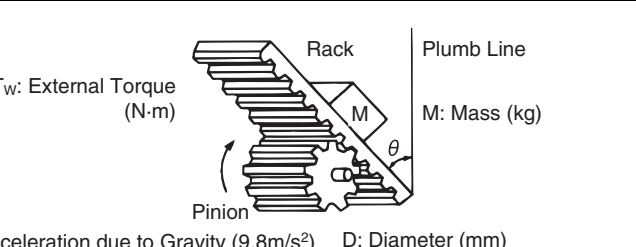
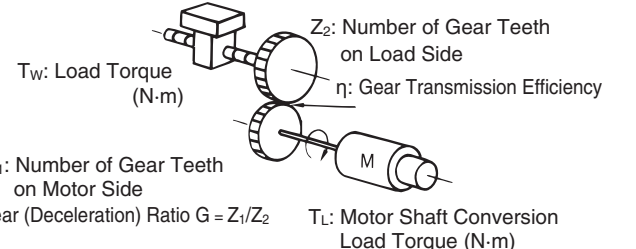
<p>Speed and Slope Trapezoid pattern</p>		<p>Conditions for Trapezoidal Operating Pattern</p> $X_0 < \frac{t_0^2 \cdot \alpha}{4}$ <p>Maximum Speed</p> $v_0 = \frac{t_0 \cdot \alpha}{2} \left(1 - \sqrt{1 - \frac{4X_0}{t_0 \cdot \alpha}} \right)$ <p>Ascending Time</p> $t_A = \frac{v_0}{\alpha} = \frac{t_0}{2} \left(1 - \sqrt{1 - \frac{4X_0}{t_0 \cdot \alpha}} \right)$ <p>X_0: Positioning Distance (mm) t_0: Positioning Time (s) t_A: Acceleration/Deceleration Time (s) v_0: Maximum Speed (mm/s) α: Speed Gradient</p>						
<p>Speed and Slope Triangular Pattern</p>		<p>Conditions for Triangular Operating Pattern</p> $X_0 \geq \frac{t_0^2 \cdot \alpha}{4}$ <p>Maximum Speed</p> $v_0 = \sqrt{\alpha \cdot X_0}$ <p>Ascending Time</p> $t_A = \sqrt{\frac{X_0}{\alpha}}$						
<p>Rotating Part</p>		<p>Perform the following unitary conversions</p> <table><tr><td>Linear Movement</td><td>Rotating Movement</td></tr><tr><td>X: Distance (mm)</td><td>θ: Angle (rad)</td></tr><tr><td>v: Speed (mm/s)</td><td>ω: Angular Velocity (rad/s)</td></tr></table> $\left(\omega = \frac{2\pi \cdot N}{60} \right)$ <p>(N: Rotating Speed (r/min))</p>	Linear Movement	Rotating Movement	X: Distance (mm)	θ : Angle (rad)	v: Speed (mm/s)	ω : Angular Velocity (rad/s)
Linear Movement	Rotating Movement							
X: Distance (mm)	θ : Angle (rad)							
v: Speed (mm/s)	ω : Angular Velocity (rad/s)							

■Inertia Formulas

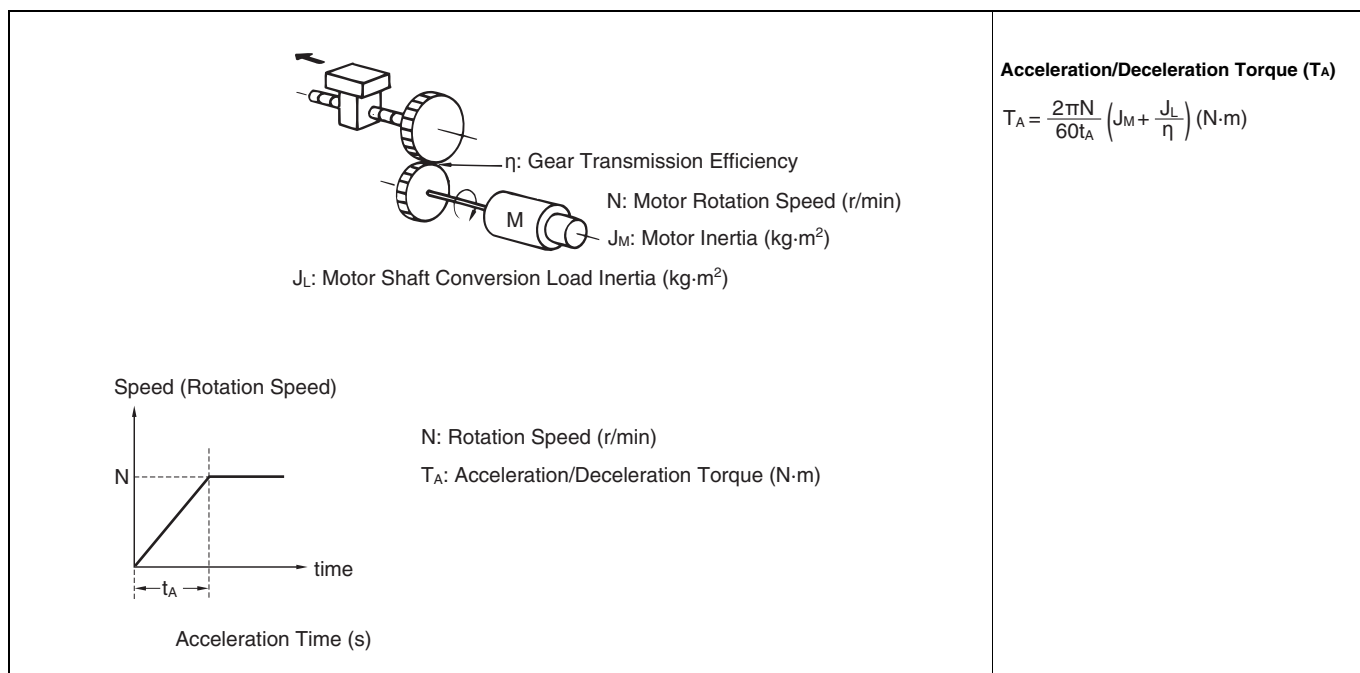
Cylindrical Inertia	 <p> D_2: Cylinder Inner Diameter (mm) D_1: Cylinder Outer Diameter (mm) M: Cylinder Mass (kg) J_W: Cylinder Inertia (kg·m²) </p>	$J_W = \frac{M (D_1^2 + D_2^2)}{8} \times 10^{-6} \text{ (kg·m}^2\text{)}$
Eccentric Disc Inertia (Cylinder which rotates off the center axis)	 <p> M: Cylinder Mass (kg) J_C: Inertia around the center axis of Cylinder J_W: Inertia (kg·m²) re: Rotational Radius (mm) Center of rotation </p>	$J_W = J_C + M \cdot re^2 \times 10^{-6} \text{ (kg·m}^2\text{)}$
Inertia of Rotating Square Cylinder	 <p> M: Square Cylinder Mass (kg) J_W: Inertia (kg·m²) L: Length (mm) a: Width (mm) b: Height (mm) </p>	$J_W = \frac{M (a^2 + b^2)}{12} \times 10^{-6} \text{ (kg·m}^2\text{)}$
Inertia of Linear Movement	 <p> M: Load Mass (kg) J_B: Ball Screw Inertia (kg·m²) P: Ball Screw Pitch (mm) J_W: Inertia (kg·m²) </p>	$J_W = M \left(\frac{P}{2\pi} \right)^2 \times 10^{-6} + J_B \text{ (kg·m}^2\text{)}$
Inertia of Lifting Object by Pulley	 <p> D: Diameter (mm) M_1: Mass of Cylinder (kg) J_1: Cylinder Inertia (kg·m²) J_2: Inertia due to the Object (kg·m²) M_2: Mass of Object (kg) J_W: Inertia (kg·m²) </p>	$J_W = J_1 + J_2 = \left(\frac{M_1 \cdot D^2}{8} + \frac{M_2 \cdot D^2}{4} \right) \times 10^{-6} \text{ (kg·m}^2\text{)}$

Inertia of Rack and Pinion Movement	 <p> J_w: Inertia (kg·m²) M: Mass (kg) D: Pinion Diameter (mm) </p>	$J_w = \frac{M \cdot D^2}{4} \times 10^{-6} \text{ (kg·m}^2\text{)}$
Inertia of Suspended Counterbalance	 <p> J_w: Inertia (kg·m²) M₁: Mass (kg) M₂: Mass (kg) </p>	$J_w = \frac{D^2 (M_1 + M_2)}{4} \times 10^{-6} \text{ (kg·m}^2\text{)}$
Inertia when Carrying Object via Conveyor Belt	<p> M₃: Mass of Object (kg) M₄: Mass of Belt (kg) </p>  <p> J_w: Inertia (kg·m²) J₁: Cylinder 1 Inertia (kg·m²) J₂: Inertia due to Cylinder 2 (kg·m²) J₃: Inertia due to the Object (kg·m²) J₄: Inertia due to the Belt (kg·m²) </p>	$J_w = J_1 + J_2 + J_3 + J_4$ $= \left(\frac{M_1 \cdot D_1^2}{8} + \frac{M_2 \cdot D_2^2}{8} \cdot \frac{D_1^2}{D_2^2} + \frac{M_3 \cdot D_1^2}{4} + \frac{M_4 \cdot D_1^2}{4} \right) \times 10^{-6} \text{ (kg·m}^2\text{)}$
Inertia where Work is Placed between Rollers	<p> J_w: System Inertia (kg·m²) J₁: Roller 1 Inertia (kg·m²) J₂: Roller 2 Inertia (kg·m²) D₁: Roller 1 Diameter (mm) D₂: Roller 2 Diameter (mm) M: Equivalent Mass of Work (kg) </p> 	$J_w = J_1 + \left(\frac{D_1}{D_2} \right)^2 J_2 + \frac{M \cdot D_1^2}{4} \times 10^{-6} \text{ (kg·m}^2\text{)}$
Inertia of a Load Value Converted to Motor Shaft	 <p> J_w: Load Inertia (kg·m²) Z₁: Number of Gear Teeth on Motor Side J₁: Gear Inertia on Motor Side (kg·m²) Gear Ratio $G = Z_1/Z_2$ Z₂: Number of Gear Teeth on Load Side J₂: Gear Inertia on Load Side (kg·m²) J_L: Motor Shaft Conversion Load Inertia (kg·m²) </p>	$J_L = J_1 + G^2 (J_2 + J_w) \text{ (kg·m}^2\text{)}$

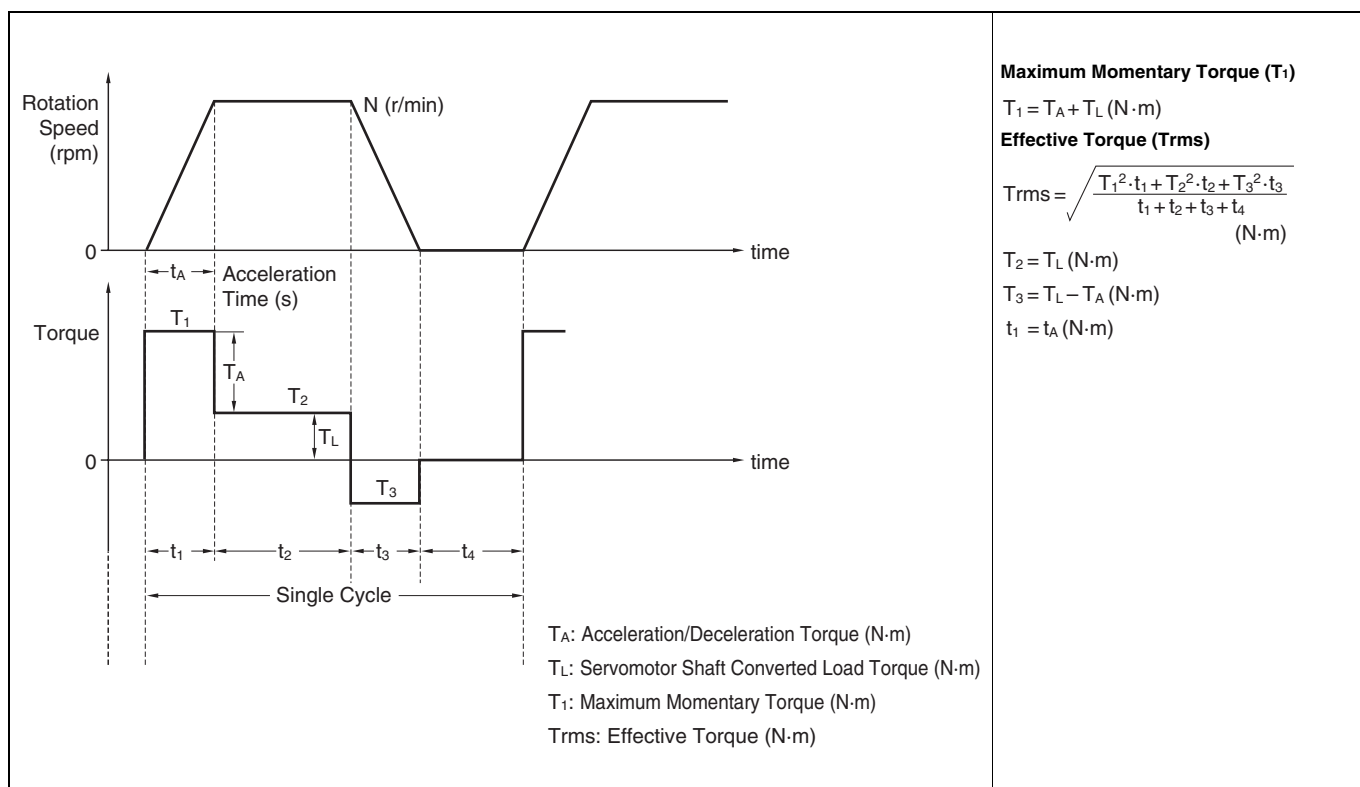
Load Torque Formulas

Torque against external force	 <p>F: External Force (N) P: Ball Screw Pitch (mm) T_w: Torque due to External Forces (N·m)</p>	$T_w = \frac{F \cdot P}{2\pi} \times 10^{-3} \text{ (N·m)}$
Torque against frictional force	 <p>M: Load Mass (kg) μ: Ball Screw Friction Coefficient P: Ball Screw Pitch (mm) g: Acceleration due to Gravity (9.8m/s²) T_w: Frictional Forces Torque (N·m)</p>	$T_w = \mu Mg \cdot \frac{P}{2\pi} \times 10^{-3} \text{ (N·m)}$
Torque when external force is applied to a rotating object	 <p>D: Diameter (mm) F: External Force (N) T_w: Torque due to External Forces (N·m)</p>	$T_w = F \cdot \frac{D}{2} \times 10^{-3} \text{ (N·m)}$
Torque of an object on the conveyer belt to which the external force is applied	 <p>D: Diameter (mm) F: External Force (N) T_w: Torque due to External Forces (N·m)</p>	$T_w = F \cdot \frac{D}{2} \times 10^{-3} \text{ (N·m)}$
Torque of an object to which the external force is applied by Rack and Pinion	 <p>F: External Force (N) D: Diameter (mm) T_w: Torque due to External Forces (N·m)</p>	$T_w = F \cdot \frac{D}{2} \times 10^{-3} \text{ (N·m)}$
Torque when work is lifted at an angle.	 <p>T_w: External Torque (N·m) Rack Pinion Plumb Line M: Mass (kg) θ g: Acceleration due to Gravity (9.8m/s²) D: Diameter (mm)</p>	$T_w = Mg \cdot \cos\theta \cdot \frac{D}{2} \times 10^{-3} \text{ (N·m)}$
Torque of a Load Value Converted to Motor Shaft	 <p>T_w: Load Torque (N·m) Z_2: Number of Gear Teeth on Load Side η: Gear Transmission Efficiency Z_1: Number of Gear Teeth on Motor Side Gear (Deceleration) Ratio $G = Z_1/Z_2$ T_L: Motor Shaft Conversion Load Torque (N·m)</p>	$T_L = T_w \cdot \frac{G}{\eta} \text{ (N·m)}$

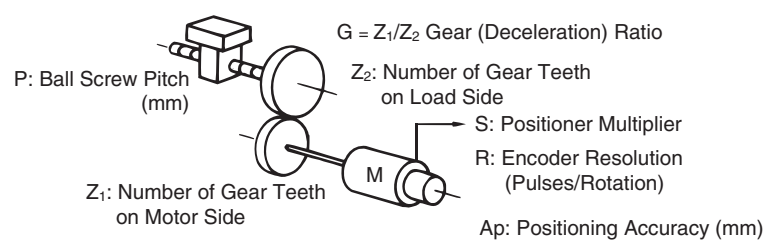
■Acceleration/Deceleration Torque Formula



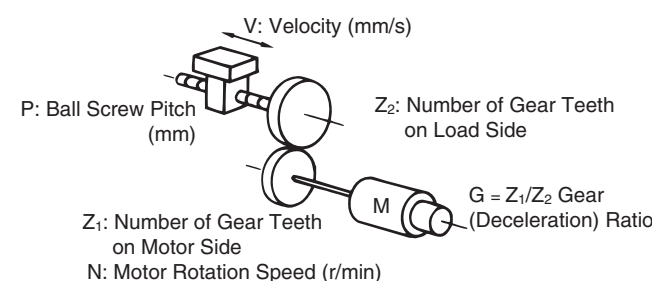
■Calculation of Maximum Momentary Torque, Effective Torque



■Positioning Accuracy

 <p>The diagram shows a motor (M) connected to a gear system. A gear with Z_1 teeth is on the motor side, and a gear with Z_2 teeth is on the load side. The gear ratio is $G = Z_1/Z_2$. A ball screw with pitch P is connected to the load side. The motor has an encoder resolution R (Pulses/Rotation). The positioner multiplier is S. The positioning accuracy is A_p (mm).</p> <p>P: Ball Screw Pitch (mm) Z_1: Number of Gear Teeth on Motor Side Z_2: Number of Gear Teeth on Load Side $G = Z_1/Z_2$ Gear (Deceleration) Ratio S: Positioner Multiplier R: Encoder Resolution (Pulses/Rotation) A_p: Positioning Accuracy (mm)</p>	<p>Positioning Accuracy (A_p)</p> $A_p = \frac{P \cdot G}{R \cdot S} \text{ (mm)}$
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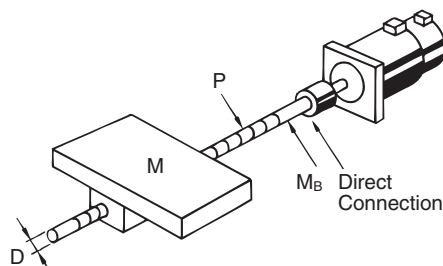
■Straight Line Speed and Motor Rotation Speed

 <p>The diagram shows a motor (M) connected to a gear system. A gear with Z_1 teeth is on the motor side, and a gear with Z_2 teeth is on the load side. The gear ratio is $G = Z_1/Z_2$. A ball screw with pitch P is connected to the load side. The motor rotation speed is N (r/min). The straight line speed is V (mm/s).</p> <p>P: Ball Screw Pitch (mm) Z_1: Number of Gear Teeth on Motor Side Z_2: Number of Gear Teeth on Load Side $G = Z_1/Z_2$ Gear (Deceleration) Ratio N: Motor Rotation Speed (r/min) V: Velocity (mm/s)</p>	<p>Motor Rotations</p> $N = \frac{60V}{P \cdot G} \text{ (r/min)}$
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Sample Calculations

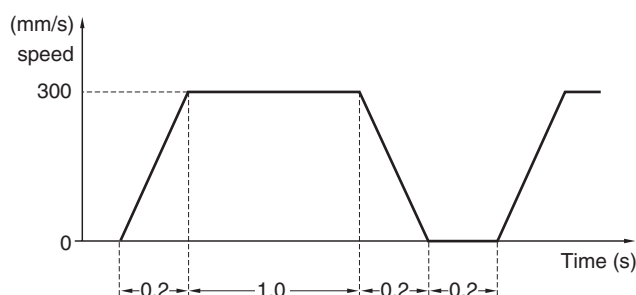
① Machinery Selection

- Load Mass $M = 5$ (kg)
- Ball Screw Pitch $P = 10$ (mm)
- Ball Screw Diameter $D = 20$ (mm)
- Ball Screw Mass $M_B = 3$ (kg)
- Ball Screw Friction Coefficient $\mu = 0.1$
- Since there is no decelerator, $G = 1$, $\eta = 1$



② Determining Operating Pattern

- One Speed Change
- Velocity for a Load Travel $V = 300$ (mm/s)
- Strokes $L = 360$ (mm)
- Stroke Travel Time $t_S = 1.4$ (s)
- Acceleration/Deceleration Time $t_A = 0.2$ (s)
- Positioning Accuracy $AP = 0.01$ (mm)



③ Calculation of Motor Shaft Conversion Load Inertia

Ball screw Inertia J_B	$J_B = \frac{M_B D^2}{8} \times 10^{-6}$	$J_B = \frac{3 \times 20^2}{8} \times 10^{-6} = 1.5 \times 10^{-4} \text{ (kg} \cdot \text{m}^2\text{)}$
Load Inertia J_W	$J_W = M \left(\frac{P}{2\pi} \right)^2 \times 10^{-6} + J_B$	$J_W = 5 \times \left(\frac{10}{2 \times 3.14} \right)^2 \times 10^{-6} + 1.5 \times 10^{-4} = 1.63 \times 10^{-4} \text{ (kg} \cdot \text{m}^2\text{)}$
Motor Shaft Conversion Load Inertia J_L	$J_L = G^2 \times (J_W + J_2) + J_1$	$J_L = J_W = 1.63 \times 10^{-4} \text{ (kg} \cdot \text{m}^2\text{)}$

④ Load Torque Calculation

Torque against Friction Torque T_W	$T_W = \mu Mg \frac{P}{2\pi} \times 10^{-3}$	$T_W = 0.1 \times 5 \times 9.8 \times \frac{10}{2 \times 3.14} \times 10^{-3} = 7.8 \times 10^{-3} \text{ (N} \cdot \text{m)}$
Motor Shaft Conversion Load Torque T_L	$T_L = \frac{G}{\eta} \cdot T_W$	$T_L = T_W = 7.8 \times 10^{-3} \text{ (N} \cdot \text{m)}$

⑤ Calculation of Rotation Speed

Rotations N	$N = \frac{60V}{P \cdot G}$	$N = \frac{60 \times 300}{10 \times 1} = 1800 \text{ (r/min)}$
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⑥ Motor Temporary Selection [In case OMNUC U Series Servo Motor is temporarily selected]

The Rotor/Inertia of the selected servo motor is more than 1/30* of a load	$J_M \geq \frac{J_L}{30}$	$\frac{J_L}{30} = \frac{1.63 \times 10^{-4}}{30} = 5.43 \times 10^{-6} \text{ (kg} \cdot \text{m}^2\text{)}$ Temporarily selected Model R88M-U20030 ($J_M = 1.23 \times 10^{-5}$).
80% of the Rated Torque of the selected servo motor is more than the load torque of the servomotor shaft conversion value	$T_M \times 0.8 > T_L$	Rated Torque for R88M – U20030 Model from TM = 0.637 (N·m) $T_M = 0.637 \text{ (N} \cdot \text{m)} \times 0.8 > T_L = 7.8 \times 10^{-3} \text{ (N} \cdot \text{m)}$

* Note that this value changes according to the Series.

⑦ Calculation of Acceleration/Deceleration Torque

Acceleration/ Deceleration Torque T_A	$T_A = \frac{2\pi \cdot N}{60 t_A} \left(J_M + \frac{J_L}{\eta} \right)$	$T_A = \frac{2\pi \times 1800}{60 \times 0.2} \times \left(1.23 \times 10^{-5} + \frac{1.63 \times 10^{-4}}{1.0} \right) = 0.165 \text{ (N}\cdot\text{m)}$
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⑧ Calculation of Maximum Momentary Torque, Effective Torque

Required Max. Momentary Torque is

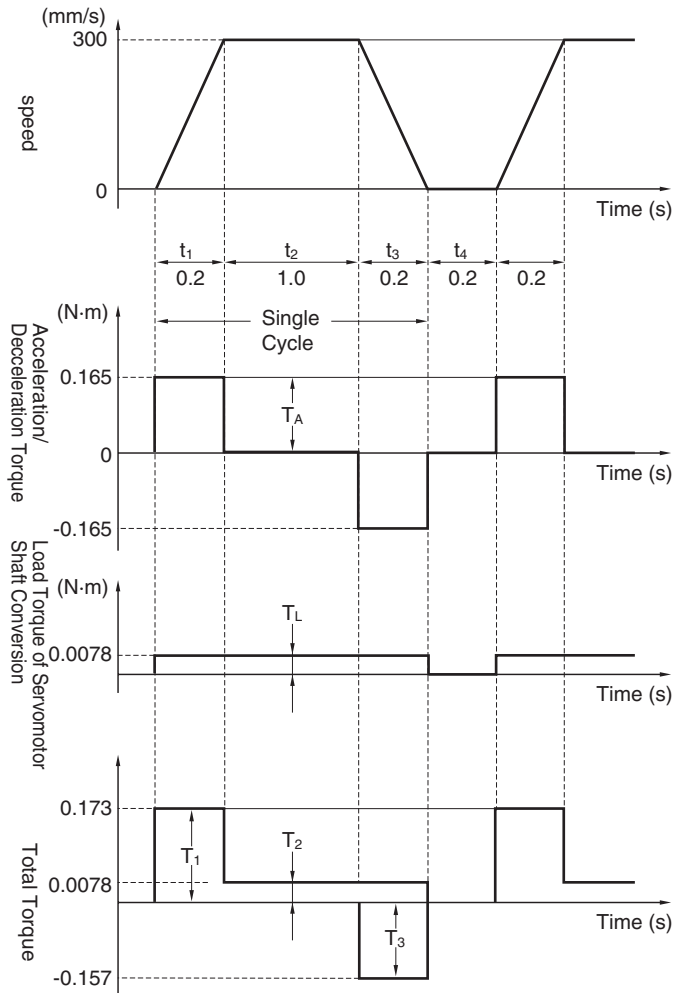
$$T_1 = T_A + T_L = 0.165 + 0.0078 \\ = 0.173 \text{ (N}\cdot\text{m)}$$

$$T_2 = T_L = 0.0078 \text{ (N}\cdot\text{m)}$$

$$T_3 = T_L - T_A = 0.0078 - 0.165 \\ = -0.157 \text{ (N}\cdot\text{m)}$$

Effective Torque Trms is

$$T_{rms} = \sqrt{\frac{T_1^2 \cdot t_1 + T_2^2 \cdot t_2 + T_3^2 \cdot t_3}{t_1 + t_2 + t_3 + t_4}} \\ = \sqrt{\frac{0.173^2 \times 0.2 + 0.0078^2 \times 1.0 + 0.157^2 \times 0.2}{0.2 + 1.0 + 0.2 + 0.2}} \\ = 0.0828 \text{ (N}\cdot\text{m)}$$



⑨ Result of Examination

Load Inertia	[Load Inertia $J_L = 1.63 \times 10^{-4} \text{ (kg}\cdot\text{m}^2\text{)}]$ \leq [Motor Rotor Inertia $J_M = 1.23 \times 10^{-5}$] \times [Applied Inertia = 30]	Conditions Satisfied
Effective Torque	[Effective Torque Trms = 0.0828 (N·m)] $<$ [Servomotor Rated Torque 0.637 (N·m) \times 0.8]	Conditions Satisfied
Maximum Momentary Torque	[Maximum Momentary Torque $T_1 = 0.173 \text{ N}\cdot\text{m}$] $<$ [Servomotor Maximum Momentary Torque 1.91 (N·m) \times 0.8]	Conditions Satisfied
Maximum Rotation Speed	[Maximum Rotations Required $N = 1800 \text{ (r/min)}$] \leq [Servomotor Rated Rotation Speed 3000 (r/min)]	Conditions Satisfied
Encoder Resolution	The encoder resolution when the positioner multiplication factor is set to 1 is $R = \frac{P \cdot G}{A_p \cdot S} = \frac{10 \times 1}{0.01 \times 1} = 1000 \text{ (Pulses/Rotations)}$ The encoder specification of U Series 2048 (pulses/rotation) should be set 1000 with the Encoder Dividing Rate Setting.	Conditions Satisfied

Note. This example omits calculations for the regenerative energy, operating conditions, or positioner characteristics.